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|-----------------|------------------|------------------|----------------|
| Project: | Job No. : | Location: | Client: |
| Sample project | 123456 | Sample location | Sample Client |

| | | |
|------------------|-------------------|----------------------------------|
| Borehole: | Soil Type: | Parameter: |
| BH1 | Coarse and Fine | Allowable Bearing Capacity (kPa) |

| Reference | Note | N | N60 | (N1)60 | Effective stress (kPa) | Depth (m) | Value | Formula |
|-----------------|--|----|-----|--------|------------------------|-----------|----------|--|
| Meyerhof Method | Based on shear failure criteria (FS = 3) B(m) = 1.50 N = Average uncorrected spt blow count to 1.5B depth below footing N = 25 CW1 = 0.77 CW2 = 1.00 | 34 | 22 | 37 | 4.95 | 0.30 | 379.5288 | $Qa(kPa) = 314.0928(NB/10(C_{w1} + C_{w2}D_f/B))/FS$ |
| | Based on shear failure criteria (FS = 3) B(m) = 1.50 N = Average uncorrected spt blow count to 1.5B depth below footing N = 23 CW1 = 0.70 CW2 = 1.00 | 12 | 8 | 14 | 10.06 | 0.61 | 398.9328 | $Qa(kPa) = 314.0928(NB/10(C_{w1} + C_{w2}D_f/B))/FS$ |
| | Based on shear failure criteria (FS = 3) B(m) = 1.50 N = Average uncorrected spt blow count to 1.5B depth below footing N = 24 CW1 = 0.63 CW2 = 1.00 | 18 | 12 | 20 | 15.02 | 0.91 | 466.5325 | $Qa(kPa) = 314.0928(NB/10(C_{w1} + C_{w2}D_f/B))/FS$ |
| | Based on shear failure criteria (FS = 3) B(m) = 1.50 N = Average uncorrected spt blow count to 1.5B depth below footing N = 24 CW1 = 0.56 CW2 = 1.00 | 26 | 17 | 29 | 20.13 | 1.22 | 518.4625 | $Qa(kPa) = 314.0928(NB/10(C_{w1} + C_{w2}D_f/B))/FS$ |
| | Based on shear failure criteria (FS = 3) B(m) = 1.50 N = Average uncorrected spt blow count to 1.5B depth below footing N = 23 CW1 = 0.50 CW2 = 0.99 | 23 | 16 | 27 | 24.88 | 1.52 | 544.2181 | $Qa(kPa) = 314.0928(NB/10(C_{w1} + C_{w2}D_f/B))/FS$ |

| Reference | Note | N | N60 | (N1)60 | Effective stress (kPa) | Depth (m) | Value | Formula |
|-----------------|--|----|-----|--------|------------------------|-----------|----------|--|
| Meyerhof Method | Based on shear failure criteria (FS = 3) B(m) = 1.50 N = Average uncorrected spt blow count to 1.5B depth below footing N = 23 CW1 = 0.50 CW2 = 0.91 | 25 | 17 | 29 | 26.96 | 1.83 | 581.5428 | $Qa(kPa) = 314.0928(NB/10(C_{w1} + C_{w2}D_f/B))/FS$ |
| | Based on shear failure criteria (FS = 3) B(m) = 1.50 N = Average uncorrected spt blow count to 1.5B depth below footing N = 23 CW1 = 0.50 CW2 = 0.85 | 39 | 27 | 46 | 28.97 | 2.13 | 617.6635 | $Qa(kPa) = 314.0928(NB/10(C_{w1} + C_{w2}D_f/B))/FS$ |
| | Based on shear failure criteria (FS = 3) B(m) = 1.50 N = Average uncorrected spt blow count to 1.5B depth below footing N = 20 CW1 = 0.50 CW2 = 0.81 | 22 | 15 | 25 | 31.05 | 2.44 | 569.5549 | $Qa(kPa) = 314.0928(NB/10(C_{w1} + C_{w2}D_f/B))/FS$ |
| | Based on shear failure criteria (FS = 3) B(m) = 1.50 N = Average uncorrected spt blow count to 1.5B depth below footing N = 19 CW1 = 0.50 CW2 = 0.77 | 21 | 16 | 26 | 33.06 | 2.74 | 570.9160 | $Qa(kPa) = 314.0928(NB/10(C_{w1} + C_{w2}D_f/B))/FS$ |
| | Based on shear failure criteria (FS = 3) B(m) = 1.50 N = Average uncorrected spt blow count to 1.5B depth below footing N = 20 CW1 = 0.50 CW2 = 0.75 | 17 | 13 | 21 | 35.24 | 3.05 | 633.4205 | $Qa(kPa) = 314.0928(NB/10(C_{w1} + C_{w2}D_f/B))/FS$ |
| | Based on shear failure criteria (FS = 3) B(m) = 1.50 N = Average uncorrected spt blow count to 1.5B depth below footing N = 19 CW1 = 0.50 CW2 = 0.72 | 18 | 13 | 20 | 37.92 | 3.35 | 631.5883 | $Qa(kPa) = 314.0928(NB/10(C_{w1} + C_{w2}D_f/B))/FS$ |

| Reference | Note | N | N60 | (N1)60 | Effective stress (kPa) | Depth (m) | Value | Formula |
|-----------------|--|----|-----|--------|------------------------|-----------|----------|--|
| Meyerhof Method | Based on shear failure criteria (FS = 3) B(m) = 1.50 N = Average uncorrected spt blow count to 1.5B depth below footing N = 20 CW1 = 0.50 CW2 = 0.70 | 20 | 15 | 23 | 40.67 | 3.66 | 697.2860 | $Qa(kPa) = 314.0928(NB/10(C_{w1} + C_{w2}D_f/B))/FS$ |
| | Based on shear failure criteria (FS = 3) B(m) = 1.50 N = Average uncorrected spt blow count to 1.5B depth below footing N = 21 CW1 = 0.50 CW2 = 0.69 | 19 | 14 | 21 | 43.34 | 3.96 | 765.1301 | $Qa(kPa) = 314.0928(NB/10(C_{w1} + C_{w2}D_f/B))/FS$ |
| | Based on shear failure criteria (FS = 3) B(m) = 1.50 N = Average uncorrected spt blow count to 1.5B depth below footing N = 21 CW1 = 0.50 CW2 = 0.68 | 25 | 19 | 28 | 46.10 | 4.27 | 799.2091 | $Qa(kPa) = 314.0928(NB/10(C_{w1} + C_{w2}D_f/B))/FS$ |
| | Based on shear failure criteria (FS = 3) B(m) = 1.50 N = Average uncorrected spt blow count to 1.5B depth below footing N = 20 CW1 = 0.50 CW2 = 0.66 | 16 | 13 | 18 | 50.82 | 4.80 | 816.6413 | $Qa(kPa) = 314.0928(NB/10(C_{w1} + C_{w2}D_f/B))/FS$ |
| | Based on shear failure criteria (FS = 3) B(m) = 1.50 N = Average uncorrected spt blow count to 1.5B depth below footing N = 21 CW1 = 0.50 CW2 = 0.65 | 22 | 18 | 25 | 52.60 | 5.00 | 879.4598 | $Qa(kPa) = 314.0928(NB/10(C_{w1} + C_{w2}D_f/B))/FS$ |
| | Based on shear failure criteria (FS = 3) B(m) = 1.50 N = Average uncorrected spt blow count to 1.5B depth below footing N = 20 CW1 = 0.50 CW2 = 0.63 | 16 | 13 | 17 | 57.94 | 5.60 | 900.3994 | $Qa(kPa) = 314.0928(NB/10(C_{w1} + C_{w2}D_f/B))/FS$ |

| Reference | Note | N | N60 | (N1)60 | Effective stress (kPa) | Depth (m) | Value | Formula |
|-------------------------------|--|----|-----|--------|------------------------|-----------|----------|--|
| Meyerhof Method | Based on shear failure criteria (FS = 3) B(m) = 1.50 N = Average uncorrected spt blow count to 1.5B depth below footing N = 18 CW1 = 0.50 CW2 = 0.63 | 26 | 22 | 28 | 61.02 | 6.00 | 848.0506 | $Qa(kPa) = 314.0928(NB/10(C_{w1} + C_{w2}D_f/B))/FS$ |
| | Based on shear failure criteria (FS = 3) B(m) = 1.50 N = Average uncorrected spt blow count to 1.5B depth below footing N = 16 CW1 = 0.50 CW2 = 0.61 | 21 | 17 | 21 | 67.18 | 6.80 | 820.8292 | $Qa(kPa) = 314.0928(NB/10(C_{w1} + C_{w2}D_f/B))/FS$ |
| | Based on shear failure criteria (FS = 3) B(m) = 1.50 N = Average uncorrected spt blow count to 1.5B depth below footing N = 14 CW1 = 0.50 CW2 = 0.60 | 15 | 12 | 14 | 73.62 | 7.50 | 769.5274 | $Qa(kPa) = 314.0928(NB/10(C_{w1} + C_{w2}D_f/B))/FS$ |
| | Based on shear failure criteria (FS = 3) B(m) = 1.50 N = Average uncorrected spt blow count to 1.5B depth below footing N = 14 CW1 = 0.50 CW2 = 0.59 | 11 | 9 | 10 | 80.45 | 8.11 | 814.2332 | $Qa(kPa) = 314.0928(NB/10(C_{w1} + C_{w2}D_f/B))/FS$ |
| | Based on shear failure criteria (FS = 3) B(m) = 1.50 N = Average uncorrected spt blow count to 1.5B depth below footing N = 16 CW1 = 0.50 CW2 = 0.59 | 16 | 13 | 14 | 84.82 | 8.50 | 963.2179 | $Qa(kPa) = 314.0928(NB/10(C_{w1} + C_{w2}D_f/B))/FS$ |
| Anagnostopoulos et al. (1991) | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average uncorrected spt blow count to 1B depth below footing N = 23 | 34 | 22 | 37 | 4.95 | 0.30 | 817.7961 | $Qa(kPa) = \left(\frac{SN^{1.2}}{2.37B^{0.7}} \right)^{1/0.87}$ |

| Reference | Note | N | N60 | (N1)60 | Effective stress (kPa) | Depth (m) | Value | Formula |
|-------------------------------|--|----|-----|--------|------------------------|-----------|------------|--|
| Anagnostopoulos et al. (1991) | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average uncorrected spt blow count to 1B depth below footing N = 21 | 12 | 8 | 14 | 10.06 | 0.61 | 721.3574 | $Qa(kPa) = \left(\frac{SN^{1.2}}{2.37B^{0.7}} \right)^{1/0.87}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average uncorrected spt blow count to 1B depth below footing N = 26 | 18 | 12 | 20 | 15.02 | 0.91 | 968.4721 | $Qa(kPa) = \left(\frac{SN^{1.2}}{2.37B^{0.7}} \right)^{1/0.87}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average uncorrected spt blow count to 1B depth below footing N = 27 | 26 | 17 | 29 | 20.13 | 1.22 | 1,020.2218 | $Qa(kPa) = \left(\frac{SN^{1.2}}{2.37B^{0.7}} \right)^{1/0.87}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average uncorrected spt blow count to 1B depth below footing N = 26 | 23 | 16 | 27 | 24.88 | 1.52 | 968.4721 | $Qa(kPa) = \left(\frac{SN^{1.2}}{2.37B^{0.7}} \right)^{1/0.87}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average uncorrected spt blow count to 1B depth below footing N = 25 | 25 | 17 | 29 | 26.96 | 1.83 | 917.4721 | $Qa(kPa) = \left(\frac{SN^{1.2}}{2.37B^{0.7}} \right)^{1/0.87}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average uncorrected spt blow count to 1B depth below footing N = 23 | 39 | 27 | 46 | 28.97 | 2.13 | 817.7961 | $Qa(kPa) = \left(\frac{SN^{1.2}}{2.37B^{0.7}} \right)^{1/0.87}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average uncorrected spt blow count to 1B depth below footing N = 20 | 22 | 15 | 25 | 31.05 | 2.44 | 674.4098 | $Qa(kPa) = \left(\frac{SN^{1.2}}{2.37B^{0.7}} \right)^{1/0.87}$ |

| Reference | Note | N | N60 | (N1)60 | Effective stress (kPa) | Depth (m) | Value | Formula |
|-------------------------------|--|----|-----|--------|------------------------|-----------|----------|--|
| Anagnostopoulos et al. (1991) | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average uncorrected spt blow count to 1B depth below footing N = 19 | 21 | 16 | 26 | 33.06 | 2.74 | 628.3445 | $Qa(kPa) = \left(\frac{SN^{1.2}}{2.37B^{0.7}} \right)^{1/0.87}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average uncorrected spt blow count to 1B depth below footing N = 20 | 17 | 13 | 21 | 35.24 | 3.05 | 674.4098 | $Qa(kPa) = \left(\frac{SN^{1.2}}{2.37B^{0.7}} \right)^{1/0.87}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average uncorrected spt blow count to 1B depth below footing N = 20 | 18 | 13 | 20 | 37.92 | 3.35 | 674.4098 | $Qa(kPa) = \left(\frac{SN^{1.2}}{2.37B^{0.7}} \right)^{1/0.87}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average uncorrected spt blow count to 1B depth below footing N = 20 | 20 | 15 | 23 | 40.67 | 3.66 | 674.4098 | $Qa(kPa) = \left(\frac{SN^{1.2}}{2.37B^{0.7}} \right)^{1/0.87}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average uncorrected spt blow count to 1B depth below footing N = 20 | 19 | 14 | 21 | 43.34 | 3.96 | 674.4098 | $Qa(kPa) = \left(\frac{SN^{1.2}}{2.37B^{0.7}} \right)^{1/0.87}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average uncorrected spt blow count to 1B depth below footing N = 20 | 25 | 19 | 28 | 46.10 | 4.27 | 674.4098 | $Qa(kPa) = \left(\frac{SN^{1.2}}{2.37B^{0.7}} \right)^{1/0.87}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average uncorrected spt blow count to 1B depth below footing N = 20 | 16 | 13 | 18 | 50.82 | 4.80 | 674.4098 | $Qa(kPa) = \left(\frac{SN^{1.2}}{2.37B^{0.7}} \right)^{1/0.87}$ |
| | | | | | | | | |

| Reference | Note | N | N60 | (N1)60 | Effective stress (kPa) | Depth (m) | Value | Formula |
|-------------------------------|--|----|-----|--------|------------------------|-----------|----------|--|
| Anagnostopoulos et al. (1991) | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average uncorrected spt blow count to 1B depth below footing N = 21 | 22 | 18 | 25 | 52.60 | 5.00 | 721.3574 | $Qa(kPa) = \left(\frac{SN^{1.2}}{2.37B^{0.7}} \right)^{1/0.87}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average uncorrected spt blow count to 1B depth below footing N = 21 | 16 | 13 | 17 | 57.94 | 5.60 | 721.3574 | $Qa(kPa) = \left(\frac{SN^{1.2}}{2.37B^{0.7}} \right)^{1/0.87}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average uncorrected spt blow count to 1B depth below footing N = 21 | 26 | 22 | 28 | 61.02 | 6.00 | 721.3574 | $Qa(kPa) = \left(\frac{SN^{1.2}}{2.37B^{0.7}} \right)^{1/0.87}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average uncorrected spt blow count to 1B depth below footing N = 16 | 21 | 17 | 21 | 67.18 | 6.80 | 495.7411 | $Qa(kPa) = \left(\frac{SN^{1.2}}{2.37B^{0.7}} \right)^{1/0.87}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average uncorrected spt blow count to 1B depth below footing N = 14 | 15 | 12 | 14 | 73.62 | 7.50 | 412.3500 | $Qa(kPa) = \left(\frac{SN^{1.2}}{2.37B^{0.7}} \right)^{1/0.87}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average uncorrected spt blow count to 1B depth below footing N = 14 | 11 | 9 | 10 | 80.45 | 8.11 | 412.3500 | $Qa(kPa) = \left(\frac{SN^{1.2}}{2.37B^{0.7}} \right)^{1/0.87}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average uncorrected spt blow count to 1B depth below footing N = 16 | 16 | 13 | 14 | 84.82 | 8.50 | 495.7411 | $Qa(kPa) = \left(\frac{SN^{1.2}}{2.37B^{0.7}} \right)^{1/0.87}$ |

| Reference | Note | N | N60 | (N1)60 | Effective stress (kPa) | Depth (m) | Value | Formula |
|------------------------------|--|----|-----|--------|------------------------|-----------|----------------|---|
| Burland and Burbridge (1985) | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average corrected spt blow count to 1.4*Br* (B/Br)^0.75 depth below footing Br = 0.3m N = 25 | 34 | 22 | 37 | 4.95 | 0.30 | 999.5698 | $Qa(kPa) = \frac{SN^{1.4}}{1.706B^{0.7}}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average corrected spt blow count to 1.4*Br* (B/Br)^0.75 depth below footing Br = 0.3m N = 24 | 12 | 8 | 14 | 10.06 | 0.61 | 944.0453 | $Qa(kPa) = \frac{SN^{1.4}}{1.706B^{0.7}}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average corrected spt blow count to 1.4*Br* (B/Br)^0.75 depth below footing Br = 0.3m N = 30 | 18 | 12 | 20 | 15.02 | 0.91 | 1,290.229 2 | $Qa(kPa) = \frac{SN^{1.4}}{1.706B^{0.7}}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average corrected spt blow count to 1.4*Br* (B/Br)^0.75 depth below footing Br = 0.3m N = 31 | 26 | 17 | 29 | 20.13 | 1.22 | 1,350.838 6 | $Qa(kPa) = \frac{SN^{1.4}}{1.706B^{0.7}}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average corrected spt blow count to 1.4*Br* (B/Br)^0.75 depth below footing Br = 0.3m N = 31 | 23 | 16 | 27 | 24.88 | 1.52 | 1,350.838 6 | $Qa(kPa) = \frac{SN^{1.4}}{1.706B^{0.7}}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average corrected spt blow count to 1.4*Br* (B/Br)^0.75 depth below footing Br = 0.3m N = 29 | 25 | 17 | 29 | 26.96 | 1.83 | 1,230.422 6 | $Qa(kPa) = \frac{SN^{1.4}}{1.706B^{0.7}}$ |

| Reference | Note | N | N60 | (N1)60 | Effective stress (kPa) | Depth (m) | Value | Formula |
|------------------------------|--|----|-----|--------|------------------------|-----------|------------|---|
| Burland and Burbridge (1985) | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average corrected spt blow count to 1.4*Br* (B/Br)^0.75 depth below footing Br = 0.3m N = 28 | 39 | 27 | 46 | 28.97 | 2.13 | 1,171.4354 | $Qa(kPa) = \frac{SN^{1.4}}{1.706B^{0.7}}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average corrected spt blow count to 1.4*Br* (B/Br)^0.75 depth below footing Br = 0.3m N = 23 | 22 | 15 | 25 | 31.05 | 2.44 | 889.4388 | $Qa(kPa) = \frac{SN^{1.4}}{1.706B^{0.7}}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average corrected spt blow count to 1.4*Br* (B/Br)^0.75 depth below footing Br = 0.3m N = 22 | 21 | 16 | 26 | 33.06 | 2.74 | 835.7740 | $Qa(kPa) = \frac{SN^{1.4}}{1.706B^{0.7}}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average corrected spt blow count to 1.4*Br* (B/Br)^0.75 depth below footing Br = 0.3m N = 23 | 17 | 13 | 21 | 35.24 | 3.05 | 889.4388 | $Qa(kPa) = \frac{SN^{1.4}}{1.706B^{0.7}}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average corrected spt blow count to 1.4*Br* (B/Br)^0.75 depth below footing Br = 0.3m N = 23 | 18 | 13 | 20 | 37.92 | 3.35 | 889.4388 | $Qa(kPa) = \frac{SN^{1.4}}{1.706B^{0.7}}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average corrected spt blow count to 1.4*Br* (B/Br)^0.75 depth below footing Br = 0.3m N = 23 | 20 | 15 | 23 | 40.67 | 3.66 | 889.4388 | $Qa(kPa) = \frac{SN^{1.4}}{1.706B^{0.7}}$ |

| Reference | Note | N | N60 | (N1)60 | Effective stress (kPa) | Depth (m) | Value | Formula |
|------------------------------|--|----|-----|--------|------------------------|-----------|----------|---|
| Burland and Burbridge (1985) | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average corrected spt blow count to 1.4*Br* (B/Br)^0.75 depth below footing Br = 0.3m N = 23 | 19 | 14 | 21 | 43.34 | 3.96 | 889.4388 | $Qa(kPa) = \frac{SN^{1.4}}{1.706B^{0.7}}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average corrected spt blow count to 1.4*Br* (B/Br)^0.75 depth below footing Br = 0.3m N = 22 | 25 | 19 | 28 | 46.10 | 4.27 | 835.7740 | $Qa(kPa) = \frac{SN^{1.4}}{1.706B^{0.7}}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average corrected spt blow count to 1.4*Br* (B/Br)^0.75 depth below footing Br = 0.3m N = 22 | 16 | 13 | 18 | 50.82 | 4.80 | 835.7740 | $Qa(kPa) = \frac{SN^{1.4}}{1.706B^{0.7}}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average corrected spt blow count to 1.4*Br* (B/Br)^0.75 depth below footing Br = 0.3m N = 23 | 22 | 18 | 25 | 52.60 | 5.00 | 889.4388 | $Qa(kPa) = \frac{SN^{1.4}}{1.706B^{0.7}}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average corrected spt blow count to 1.4*Br* (B/Br)^0.75 depth below footing Br = 0.3m N = 22 | 16 | 13 | 17 | 57.94 | 5.60 | 835.7740 | $Qa(kPa) = \frac{SN^{1.4}}{1.706B^{0.7}}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average corrected spt blow count to 1.4*Br* (B/Br)^0.75 depth below footing Br = 0.3m N = 24 | 26 | 22 | 28 | 61.02 | 6.00 | 944.0453 | $Qa(kPa) = \frac{SN^{1.4}}{1.706B^{0.7}}$ |
| | | | | | | | | |

| Reference | Note | N | N60 | (N1)60 | Effective stress (kPa) | Depth (m) | Value | Formula |
|-----------------------------|--|----|-----|--------|------------------------|-----------|----------|---|
| Burland and Burbidge (1985) | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average corrected spt blow count to 1.4*Br* (B/Br)^0.75 depth below footing Br = 0.3m N = 15 | 21 | 17 | 21 | 67.18 | 6.80 | 488.9054 | $Qa(kPa) = \frac{SN^{1.4}}{1.706B^{0.7}}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average corrected spt blow count to 1.4*Br* (B/Br)^0.75 depth below footing Br = 0.3m N = 13 | 15 | 12 | 14 | 73.62 | 7.50 | 400.1454 | $Qa(kPa) = \frac{SN^{1.4}}{1.706B^{0.7}}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average corrected spt blow count to 1.4*Br* (B/Br)^0.75 depth below footing Br = 0.3m N = 12 | 11 | 9 | 10 | 80.45 | 8.11 | 357.7263 | $Qa(kPa) = \frac{SN^{1.4}}{1.706B^{0.7}}$ |
| | Based on allowable settlement (25.00mm) B(m) = 1.50 N = Average corrected spt blow count to 1.4*Br* (B/Br)^0.75 depth below footing Br = 0.3m N = 14 | 16 | 13 | 14 | 84.82 | 8.50 | 443.8910 | $Qa(kPa) = \frac{SN^{1.4}}{1.706B^{0.7}}$ |